

Mark schemes

Q1.

$$\text{amount of CaS} = \frac{2.50}{72.2} = 0.0346 \text{ mol}$$

M1: amount of CaS

1

$$\text{amount of CaSO}_4 = \frac{9.85}{136.2} = 0.0723 \text{ mol}$$

M2: amount of CaSO₄

1

3 mol of CaSO₄ needed for each mol of CaS, and n(CaSO₄) is not 3 × n(CaO)
(so CaSO₄ is the limiting reagent)

M3: limiting reagent justification

1

$$n(\text{SO}_2) = n(\text{CaSO}_4) \times \frac{4}{3} = 0.0964 \text{ mol}$$

M4: moles of CaSO₄ × 4/3

1

$$\text{mass of SO}_2 = n(\text{SO}_2) \times 64.1 = 6.18 \text{ g}$$

M5: M4 × 64.1

If CaS used as limiting reagent then allow M4 and M5 ecf.

Must look for M1 and M3

1

[5]

Q2.

(a) *M1: Mean titre = $\frac{20.25+20.30}{2} = 20.275 \text{ cm}^3$*
Allow M1 = 20.28 cm³

1

M2 Amount of NaOH = 0.35 × (20.275 ÷ 1000) = 0.00709625 mol

Amount of ethanoic acid in 25 cm³ = 0.00709625 mol

M2 = M1 × 10⁻³ × 0.35

1

M3 Amount of ethanoic acid in 200 cm³ = 0.05677 mol

M3 = M2 × 8

1

M4 Mass of ethanoic acid in sample = 60.0 × 0.05677 = 3.4062 g

M4 = M3 × 60.0

1

$$M5 \text{ Mass of sodium ethanoate} = 5.6 - 3.4062 = 2.1938 \text{ g}$$

$$M5 = 5.6 - M4$$

1

$$M6 \text{ percentage } \text{CH}_3\text{COONa} = (2.1938 \div 5.6) \times 100 = 39.1 \%$$

$$M6 = (M5 \div 5.6) \times 100$$

$$(39.1 - 39.2)$$

Accept alternative methods

$$M5 = (M4 \div 5.6) \times 100 \text{ followed by } M6 = 100 - M5$$

1

1

(b) M1 Titre value would increase / larger value

1

M2 Because the sodium hydroxide solution would be more dilute

1

[8]

Q3.

(a) **METHOD 1**

Stage 1

$$M1 \quad n = \frac{PV}{RT}$$

1

M2 converting P to 51.0×10^3 , V to 482×10^{-6}

1

$$M3 \quad \frac{51.0 \times 10^3 \times 482 \times 10^{-6}}{8.31 \times 297} (= 0.00996)$$

1

Stage 2

M4 converting mass to 0.717

1

$$M5 \quad M_r \left(= \frac{\text{mass}}{\text{moles}} \right) = \frac{M4}{M3} = 72.0 \text{ (at least 2 sf)}$$

1

METHOD 2

$$M1 \quad n = \frac{PV}{RT}$$

$$M2 \quad M_r = \frac{mRT}{PV}$$

M3 converting P to 51.0×10^3 , V to 482×10^{-6}

M4 converting mass to 0.717

$$\mathbf{M5} \quad M_r = \left(\frac{0.717 \times 8.31 \times 297}{51.0 \times 10^3 \times 482 \times 10^{-6}} \right) = 72.0 \text{ (at least 2 sf)}$$

Both methods:

72.0 can be achieved with incorrect working and may not score because individual steps need to be assessed as correct

72.0 with no working scores no marks

*If expression not written out, **M1** could score from a substituted correct expression later on (even if any unit conversions are incorrect)*

METHOD 1

- ECF from **M2** to **M3**
- ECF from **M3** to **M4**
- ECF from **M4** to **M5**
- Ignore units for **M3**

METHOD 2

- ECF from **M3** to **M4**
- ECF from **M2** to **M4**
- ECF from **M4** to **M5**

(b) **M1** amount of CO₂ formed in flask = 0.008 mol

*Allow ECF from **M1** to **M2***

1

M2 amount of gas in flask

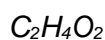
$$= 0.0075 (\text{O}_2) + 0.0080 (\mathbf{M1}) = 0.0155 \text{ mol}$$

1

[7]

Q4.

C



[1]

Q5.

B

$$1.74 \times 10^{-2}$$

[1]

Q6.

C

$$51.1\%$$

[1]

Q7.

C

1.47

[1]

Q8.

B

ethanol

[1]

Q9.

(a) M1 $n = pV / RT$ *M1 for rearrangement*

$$n = \frac{100000 \times (178/1000000)}{8.31 \times (273 + 120)}$$

M2

*M2 for three unit conversions*M3 $n = 5.45 \times 10^{-3}$ mol

$$M_r = \text{mass/mol or } 0.460 / 5.45 \times 10^{-3}$$

*M3 for calculating the amount in moles of A*M4 $M_r = 84.4$ Answer must be to 3 sig.fig.*M4: 0.460 / M3 given to 3sf*

4

(b) Calculated M_r value would be greater than actual *$M_r = \text{mass} / \text{moles}$ so dividing by too small a value of moles gives a larger M_r than expected.*

1

A lower volume would have been recorded / mass evaporated less than mass of liquid / lower moles calculated / mass recorded higher than mass of gas / mass recorded would be too high

M2 dependent on correct M1

1

(c) % uncertainty = (uncertainty / mass added) x 100

$$= ((2 \times 0.001) / 0.460) \times 100 = 0.435\%$$

1

[7]

Q10.

Percentage yield

$$\text{M1 reactant moles} = \frac{1.00}{116.0} (= 0.00862)$$

Correct **M3** scores **M1-3**

Numerical answers to at least 2sf

Allow ECF in **M1-M3**

1

M2 product moles = $\frac{0.552}{72.0}$ (= 0.00767)

Alternative for M2/3

M2 expected mass of product = 0.00862×72.0 (= 0.621 g)

1

M3 % yield = $\frac{0.00767}{0.00862} = 88.9(3)$ or 89%

Alternative for M2/3

M3 % yield = $\left(\frac{0.552}{0.621} \times 100\right) = 88.9(3)$ or 89%

1

M4 idea of getting as much product as possible in the reaction / idea of efficient conversion of reactants to products

1

Atom economy

M5 $\left(\frac{72.0}{74.0+34.0} \times 100\right) = \left(\frac{72.0}{108.0} \times 100\right) = 66.7\%$

Alternative for M5: $\left(\frac{72.0}{72.0+36.0} \times 100\right)$

1

M6 idea of maximising the mass of reactants / atoms that ends up in desired product or idea of minimising the amount of by-products

1

[6]

Q11.

(a) **M1** $n(\text{S}_2\text{O}_3^{2-}) = 33.50 \times 0.100 \div 1000 = \underline{0.00335}$

1

M2 $n(\text{I}_2) = 0.00335 \div 2 = 0.001675$ (from eqn 2)

M2 = M1 ÷ 2

1

M3 $n(\text{ClO}^-)$ in 25 cm³ pipette = 0.001675 (from eqn 1)

M3 = M2

1

M4 $n(\text{ClO}^-)$ in 100 cm³ flask = 0.001675 **x 4** = 0.00670 = $n(\text{NaClO})$ in original 10 cm³ sample

M4 = M3 x 4

1

M5 mass (NaClO) = $0.00670 \times 74.5 = 0.499 \text{ g}$
M5 = $M4 \times 74.5$

1

M6 mass (bleach) = $10.0 \times 1.20 = 12 \text{ g}$
M6 = mass of bleach

1

M7 % by mass of NaClO = $\frac{0.499}{12} = 4.16 \%$
M7 = $(M5 \div M6) \times 100$ to 3 significant figures
 Allow 4.15% to 4.17%

1

(b) 0.45%

1

[8]

Q12.

C

[1]

Q13.

A

$$2.28 \times 10^{-18} \text{ J}$$

[1]

Q14.

(a) $M_r \text{ NaF} = 42(.0)$

Incorrect M_r loses M1 & M4

1

Mass NaF in 1 g = $2.88 \times 10^{-5} \times 42.0 = 1.210 (1.2096) \times 10^{-3} \text{ g}$

1

Mass NaF in 1 kg = $1.210 (1.2096) \text{ g}$

$$M3 = M2 \times 1000 \text{ (g)}$$

Units, if given, must match answer

1

(Mass in mg = $1210 (1209.6) \text{ mg}$)

Concentration of NaF = 1210 (ppm)

Allow $1.21 \times 10^3 \text{ ppm}$

1

(b) Toxic mass = $3.19 \times 10^{-2} \times 75 \times 1000$
 = 2390 mg
 Allow 2393

1

(c) Mass of toothpaste needed = $\frac{2390}{2800}$
= 0.854 kg

Mark consequential to (b)

(b) \div 2800 (to at least 2 sig fig)

Allow 0.85 - 0.86 kg

1

(d) B

If not B, allow M2 only

If blank, read on.

1

Both Na⁺ and F⁻ same electron arrangement (1s²2s²2p⁶) or isoelectronic

Electronegativity, molecules or IMF = CE, M1 only

1

Sodium (ion) has more protons so attracts (outer) electrons closer /

Sodium (ion) has more protons so stronger attractions for (outer) electrons

Ignore shielding, higher charge density, atomic radius

If reference to fluorine rather than fluoride, then penalise 1 mark only

1

[9]

Q15.

(a) **M1:** Mass Na₂CO₃ = 0.57g AND Mass H₂O = 0.55g

If incorrect masses other than AE, lose M1 & M3

1

M2: Mol Na₂CO₃ = $\frac{0.57}{106}$ AND Mol H₂O = $\frac{0.55}{18}$

M2 = process

1

M3: = 0.0054 : 0.0306

M3 = these values only (at least 2sf)

1

M4: \div by smallest = 1 : 5.682

M4 = process mark

1

M5: Value of x = 5.68 (2dp)

Allow 5.67 – 5.74

1

OR

M1: Mass Na₂CO₃ = 0.57g AND Mass Na₂CO₃.xH₂O = 1.12g

1

$$\text{M2: Moles anhydrous Na}_2\text{CO}_3 = \frac{0.57}{106} = 5.377 \times 10^{-3}$$

1

$$\text{M3: Mr of hydrated Na}_2\text{CO}_3 = 1.12 / 5.377 \times 10^{-3} \\ = 208.3$$

1

$$\text{M4: Mr of } x \text{ H}_2\text{O} = 102.3$$

1

$$\text{M5: Value of } x = 5.68 \text{ (2dp)} \\ \text{Allow } 5.67 - 5.74$$

1

- (b) Failure to drive off all the water
OR
Failure to heat for long enough
OR
Not heated to constant mass

Allow evaporate instead of drive off
Ignore incomplete reaction

1

- (c) Heat to constant mass / heat for longer / use a smaller mass

1

You can be sure all / more of the water has been driven off
Ignore incomplete reaction
M2 dependent on M1

1

[8]

Q16.

- (a) The sum of $\frac{\text{(weighted) average masses of atoms in formula}}{1/12 \text{ mass of an atom of } ^{12}\text{C}}$
 $\frac{\text{Average mass of one molecule}}{1/12 \text{ mass of an atom of } ^{12}\text{C}}$

1

Method 1

$$\text{Mass of Y} = 0.21\text{g}$$

Method 2

$$\text{Mass of Y} = 0.21\text{g}$$

If incorrect lose M5 also, unless AE

1

$$M_r = \frac{mRT}{pV}$$

$$n = \frac{pV}{RT} \text{ and } M_r = \frac{m}{n}$$

Can be implied in calculations

1

$$M_r = \frac{0.21 \times 8.31 \times 371.1}{102000 \times 85 \times 10^{-6}} \quad n = \frac{102000 \times 85 \times 10^{-6}}{8.31 \times 371.1} (= 2.81 \times 10^{-3})$$

M4 – awarded for all 3 unit conversions

1

$$M_r = 74.7 \quad M_r = 74.7$$

Allow 75

1

- (b) Lower volume recorded

Allow

(Evaporated) mass of gas is less than the recorded mass of liquid / 0.21g (or converse)

1

M_r would be greater (than the real M_r)

Ignore other references to mass

1

[7]

Q17.

C

[1]

Q18.

D

[1]

Q19.

- (a) use of water would dilute the NaOH OR
use of water would change the concentration of NaOH OR
to ensure the concentration of the NaOH is not changed OR

*Ignore reference to weakening the solution,
watering down the solution, contaminate*

Allow

it would give a titre value that is larger

it would decrease the pH of the NaOH

(any additional qualifying reason given must be correct)

1

- (b) Rough = 25.2, 1 = 23.90, 2 = 23.70, 3 = 24.00.

Need all four (with rough to 1dp and the other three to 2dp)

1

- (c) **M1** use of titrations 1 & 3 only

M1 is for choosing correct titres

1

M2 23.95 (cm³)

M2 is for calculating the mean to 2dp for their chosen titres

24.0 cm³ = 1 mark (wrong number of decimal places)

24 cm³ = 1 mark (only if it is clear that titration 2 is not included)

23.86 cm³ = 1 mark (used all three titrations)

23.9 cm³ = 0 marks (used all three titrations and wrong number of decimal places)

If error(s) made in 2.2, allow ECF from 2.2, where they choose concordant titres and find the mean (can score M1 and M2)

1

(d) $\frac{0.15}{23.95} \times 100 = 0.63\%$
(0.6263%)

Allow any correct value with at least 2 significant figures based on their answer to 2.3. Rounding must be correct.

1

(e) **M1** moles NaOH = $\frac{23.95}{1000} \times 0.0500 (=0.001198)$

1

M2 moles acid in flask = $\frac{M1}{3} \times 10 (= 0.003992)$

1

M3 mass acid (= 0.003992 x 192.0 = 0.766 g) = 766 (mg)
Correct answer to at least 2sf = 3 marks (allow 760-770 mg)
Correct value in grams (lose M3) = 2 marks (allow 0.76-0.77 g)
Allow ECF at each stage (including those based on value from 2.3)
Incorrect answers that are a factor of 10 too small lose M2 (76-77 mg = 2 marks, 0.076-0.077 g = 1 mark)
(if use 25 cm³ for volume of NaOH, then max 2 marks (**M2** and **M3** for 800 mg)

1

(f) $\frac{\text{Answer to Q (e)}}{784} \times 100 = 97.7$ or 97.8%

Allow any correct value to at least 2 significant figures based on their answer to Q(e)
(values may be over 100% if 2.5 is incorrect)

1
[9]**Q20.**

- M1** HCl added = 0.050 mol and
NaOH used in titration = 3.99×10^{-3} mol
1
- M2** So moles that would be needed to neutralise total excess
HCl = $3.99 \times 10^{-3} \times 10 = 3.99 \times 10^{-2}$ mol
*Alternative: divide moles HCl by 10 = 0.005 and
 $0.005 - 3.99 \times 10^{-3} = 0.00101$*
1
- M3** Therefore the moles of HCl reacted with the $\text{Na}_2\text{CO}_3 \cdot x\text{H}_2\text{O} =$
 $0.050 - 3.99 \times 10^{-2} = 0.0101$ mol
Alternative: 0.00101×10 to produce 0.0101
1
- M4** So moles $\text{Na}_2\text{CO}_3 \cdot x\text{H}_2\text{O}$ reacted with the HCl = $0.0101 / 2 = 5.05 \times$
 10^{-3} mol
1
- M5** Conversion of mg to g = 0.627 (g) or 627×10^{-3} (g)
1
- M6** $x\text{H}_2\text{O} = 0.627 / 5.05 \times 10^{-3} - 106.0 = 18$ (.16)
*Alternative: mass Na_2CO_3 that reacted with the
HCl $5.05 \times 10^{-3} \times 106.0 = 0.5353$ g and mass $\text{H}_2\text{O} =$
 $0.627 - 0.5353 = 0.0917$ g*
1
- M7** so $x = \underline{1}$
*Alternative: $0.0917 / 18.0 = 5.094 \times 10^{-3}$ so ratio
 Na_2CO_3 to $\text{H}_2\text{O} = 1:1.009$ ie 1:1 so $x = 1$*
1

[7]

Q21.

- (a) $4\text{CuFeS}_2 + \frac{1}{92}\text{O}_2 + 4\text{SiO}_2 \rightarrow \text{Cu}_2\text{S} + \text{Cu}_2\text{O} + 7\text{SO}_2 + 4\text{FeSiO}_3$
Allow multiples
1
- $\text{Cu}_2\text{S} + 2\text{Cu}_2\text{O} \rightarrow 6\text{Cu} + \text{SO}_2$
1
- (b) ANY TWO
- Prevents acid rain (which damages buildings / ecology)
 - Toxic OR causes breathing problems
 - Reduces waste product OR makes use of the waste OR improves atom economy OR Reduces need for sulfur mining OR used to produce sulfuric acid OR any named products

2

(c) M1, M2, M3 are process marks

$$\text{M1} \quad \text{Mol Cu} = \frac{450 \times 1000}{63.5} (= 63780)$$

1

$$\text{M2} \quad \text{Mass CuFeS}_2 = (63780) \times 183.5 (= 1.17 \times 10^7\text{g})$$

1

$$\text{M3} \quad \text{Mass ore} = (1.17 \times 10^7) \times \frac{100}{1.25}$$

1

$$\text{M4} \quad \text{Mass ore} = 936 \text{ tonnes (Allow } 936 - 937)$$

1

Alternative method

$$\text{M1} \quad \% \text{ of Cu in CuFeS}_2 = (63.5/183.5) \times 100 = 34.6\%$$

$$\text{M2} \quad \% \text{ of Cu in the rock} = (34.6/100) \times 1.25 = 0.4325\%$$

$$\text{M3} \quad \text{mass of rock} = 4050 \times 100/0.4325 = 936416\text{kg}$$

$$\text{M4} \quad \text{mass of rock in tonnes} = 936 \text{ tonnes}$$

NotesM1 A_r Cu must be usedM2 M_r CuFeS₂ to have been used

M3 Grossing up for the mass of rock

M4 Final answer correct in tonnes

$$\text{(d)} \quad \% \text{ atom economy} = \frac{(2 \times 63.5)}{171} \times 100$$

1

$$= 74.3\% \text{ must be 3sf}$$

1

[10]

Q22.

D

[1]

Q23.

B

[1]

Q24.(a) **Stage 1**

$$\text{M1} \quad n = \frac{PV}{RT}$$

1

$$\text{M2} \quad = \frac{102 \times 10^3 \times 72 \times 10^{-6}}{8.31 \times 373}$$

1

$$\mathbf{M3} = 0.0024 / 0.00237 / 0.002369 / 0.0023693 ..$$

1

Stage 2

$$\mathbf{M4} \quad M_r (= \frac{\text{mass}}{\text{moles}}) = \frac{0.194}{\mathbf{M3}}$$

1

$$\mathbf{M5} = 82 \text{ (2sf only)}$$

1

As this is an extended response question, each separate step of correct working is required in **M1–M5**

Correct answer with no working scores 2 marks

M1 – If expression not written out, **M1** could score from a correct expression for **M2** (even if unit conversions are not correct for **M2**)

M2 – allow an expression that gives correct value for **M3**

M3 should be at least 2sf (do not allow 0.0023 but do allow 0.00236)

M4 must show 0.194 or 194×10^{-3} in working to score

M5 must be 2sf

ECF:

- No ECF within either stage 1 or stage 2 (except for transcription errors)
- Allow ECF from stage 1 into stage 2, i.e for **M4** and **M5** based on incorrect **M3**, (but if expression for **M4** is inverted, cannot score **M5**)
- (Note that if 72×10^{-3} used in **M2**, then **M3** = 2.4, **M5** = 0.082)

Ignore units for **M3** and **M5**

Note that if $T = 273 + 373 = 646$, **M5** = 140 (2sf)

(b) **M1** dividing %s by relative atomic masses
C = $83.7/12(.0)$, H = $16.3/1(.0)$

1

M2 converting (C : H 6.975 : 16.3) to 3 : 7

1

M3 empirical formula = C_3H_7

1

M4 molecular formula = C_6H_{14}

1

M1 & **M2** are for working

M3 for C_3H_7 only, marked independently

M4 for C_6H_{14} only, marked independently (ignore additional correct structures)

Formulae with no working cannot score **M1** or **M2**

Alternative method:

M1 working that shows 83.7% of 86 is 72

M2 idea of 72/12 gives 6 C atoms

Alternative method:

working that shows that C_6H_{14} (or C_3H_7) contains 83.7% C scores **M1 & M2**

[9]

Q25.

- (a) **M1** Amount NaOH = $0.02530 \times 0.500 = 0.01265$ mol
 567-590 = 4 marks
 0.567-0.590 = 3 marks 1
- M2** Amount acid = 0.006325 mol (i.e. **M1** \div 2)
 Allow ECF at each stage 1
- M3** $M_r = 90(.0)$
M3 can be scored from use of value of 90(.0) within working 1
- M4** mass acid = 569 (mg) (allow 567 to 576) (i.e. **M2** \times **M3** in mg)
M4 should be to at least 2sf. Any individual marks for **M1/2/3** should be to at least 2sf (or 90 for **M3**) 1
- 1134-1180 = 3 marks (due to not dividing moles of NaOH by 2)
 1.134-1.180 = 2 marks (due to not dividing moles of NaOH by 2 and not converting to mg)
- (b) Idea that it ensures all ethanedioic acid / acid / sodium hydroxide / alkali / reactants are in the mixture / solution / reaction or the idea that some of the ethanedioic acid / acid / sodium hydroxide / alkali / reactants would be on the sides of the flask
 the idea that it is the transfer of all the acid/alkali alone is not enough 1
- (c) Titres that are within 0.1 cm³ of each other
 Units are needed
 Allow 0.05-0.15 cm³
 Do not allow idea of identical results
 Allow answers that refer to titres that are within the uncertainty of the burette/apparatus of each other 1

[6]

Q26.

- (a) Mass of **X** = 0.270
 Volume of **X** = 105.0

Both must be correct

1

(b) $pV = nRT$

$$\frac{100\,000 \times 105 / 1000000}{8.31 \times 370} = n$$

1

$$n = 3.41 \times 10^{-3}$$

1

$$M_r = \frac{\text{mass}}{\text{mol}} \quad \text{or} \quad \frac{0.270}{3.41 \times 10^{-3}}$$

1

$$M_r = 79.1$$

1

Identity of **X** = CH₂Cl₂

If $M_r = 52$ used, allow CH₃Cl

1

- (c) **M1** The volume of the gas in the syringe (V) is greater than the true volume (because some air leaked into the syringe)

If the M_r value of 52 is used and CH₃Cl is identified in 01.2:

1

M2 $M_r = m/n = m \times RT/PV$ so if V is too large, M_r is too small

OR

M1 The temperature measured (T) is less than the temperature of the gas in the syringe (because the syringe heated faster than the oven and the oven temperature was not constant)

M2 $M_r = m/n = m \times RT/PV$ so if T is too small, M_r is too small

OR

M1 The measured mass of liquid transferred to the syringe (m) is less than the actual mass transferred

M2 $M_r = m/n = m \times RT/PV$ so if m is too small, M_r is too small

M1 *The volume of the gas in the syringe (V) is less than the true volume (because not all the liquid vaporised in the syringe)*

M2 *$M_r = m/n = m \times RT/PV$ so if V is too small, M_r is too large*

OR

M1 *The temperature measured (T) is greater than the temperature of the gas in the syringe (because the syringe heated more slowly than the*

thermometer and the oven temperature was not constant)

M2 $M_r = m/n = m \times RT/PV$ so if T is too large, M_r is too large

OR

M1 *The measured mass of liquid transferred to the syringe (m) is greater than the actual mass transferred*

M2 $M_r = m/n = m \times RT/PV$ so if m is too large, M_r is too large

1

(d) Carry out in a fume cupboard

Do not allow safety glasses / labcoat

1

To avoid toxic vapour

1

[10]

Q27.

D

[1]